

1 Direct measurement of ammonia in simulated human breath using an inkjet-printed
2 polyaniline nanoparticle sensor

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10 Abstract

11 A sensor fabricated from the inkjet-printed deposition of polyaniline nanoparticles onto a
12 screen-printed silver interdigitated electrode was developed for the detection of ammonia
13 in simulated human breath samples. Impedance analysis showed that exposure to
14 ammonia gas could be measured at 962 Hz at which changes in resistance dominate due
15 to the deprotonation of the polymer film. Sensors required minimal calibration and
16 demonstrated excellent intra-electrode baseline drift ($\leq 1.67\%$). Gases typically present in
17 breath did not interfere with the sensor. Temperature and humidity were shown to have
18 characteristic impedimetric and temporal effects on the sensor that could be distinguished
19 from the response to ammonia. While impedance responses to ammonia could be detected
20 from a single simulated breath, quantification was improved after the cumulative
21 measurement of multiple breaths. The measurement of ammonia after 16 simulated

22 breaths was linear in the range of 40 to 2,175 ppbv (27 to 1,514 $\mu\text{g}/\text{m}^3$) ($r^2=0.9963$) with a
23 theoretical limit of detection of 6.2 ppbv (4.1 $\mu\text{g}/\text{m}^3$) (S/N=3).

24

25 Key Words

26 Ammonia, Breath, Impedance, Polyaniline, Nanoparticle, Inkjet

27

28 1. Introduction

29

30 The provision of real-time, point-of-care diagnostic and analytical information in a non-
31 invasive manner is a major goal of modern biomedical diagnostics. There are several
32 routes to non-invasive or minimally invasive measurements. One extremely attractive
33 route is exhaled breath. Extensive research has shown that links exist between breath gas
34 concentrations and pathologies of the human body. For example, excessive levels of
35 acetone have been shown to correlate with the incidence of diabetes [1], while breath
36 formaldehyde levels have been linked with cancer [2]. Another volatile breath gas of
37 interest is ammonia, and its potential link with dysfunctions of the kidneys and liver [3].
38 Ammonia is produced as part of the process of nitrogen metabolism and is eventually
39 converted to urea and excreted from the body as part of the urea cycle [4]. Significant
40 quantities of ammonia are also produced by intestinal flora which must also be detoxified
41 by the liver. In instances of liver dysfunction, or in some rare genetic disorders in which
42 ammonia is not metabolised correctly, blood ammonia levels may become elevated. In

43 some cases, this becomes toxic, leading to hepatic encephalopathy. Here, ammonia
44 crosses the blood-brain barrier, leading to cognitive impairment, coma and, in extreme
45 cases even death [5]. In cases of kidney dysfunction, ammonia, urea and other forms of
46 blood nitrogen such as creatinine are not excreted effectively and these levels rise in
47 blood, while urea is also converted back to ammonia by the gut flora. Current established
48 methods for measuring blood nitrogen levels are invasive, requiring blood sampling.
49 However, it has been well-established that elevation of ammonia concentrations in blood
50 in turn leads to an increase in its rate of gaseous exchange in the lungs and its elevation in
51 exhaled breath [6]. Exhaled human breath consists predominantly of nitrogen, oxygen,
52 carbon dioxide and inert gases,[7] as well as water vapour at a relative humidity (RH)
53 between 91 to 96% [8]. In addition, it can contain in excess of 1,000 volatile compounds,
54 including ammonia [9]. The level of ammonia in human breath has been measured as
55 being between 50 ppbv (where 1 ppbv of ammonia in human breath is approximately 0.67
56 $\mu\text{g}/\text{m}^3$) and several thousand ppbv and is dependent on a range of factors including the
57 health status of the patient, the route of sampling (nasal or oral), contribution from oral
58 bacteria, as well as diet, pharmaceutical use and levels of metabolic activity [10]. Thus,
59 the diagnostic measurement of ammonia in human breath must be capable of measuring
60 ammonia in this concentration range, while also being free from interference from other
61 breath constituents. While it is critical to assess the performance of any analytical device
62 in the real sample matrix, the lack of the ready availability of human breath as well as the
63 natural variation of human breath samples leads logically to the use of a source of
64 simulated breath that replicates the major features of natural breath samples with known
65 concentrations of trace ammonia at diagnostically relevant concentrations, while being in
66 constant and convenient availability in the laboratory [11].

67 A range of methods have been developed for measuring ammonia in human breath [12]
68 and the most successful of these have been instrumental methods such as selective ion
69 flow tube mass spectroscopy (SIFT-MS) and photoacoustic laser spectroscopy (PALS).
70 These systems can directly measure ammonia in human breath down to ppbv levels
71 without interference and in 'real time'. SIFT-MS can also be used to measure a whole
72 host of other volatile trace gases in breath and is an excellent laboratory research tool.
73 However, these systems are large and expensive and are not suitable for translation into
74 application in biomedical diagnostics where 'point of care' type technologies are
75 required.

76 A number of sensor and microsystems approaches have also been developed for
77 measuring breath ammonia. Timmer *et al.* developed a microfluidic system to measure
78 ammonia using a conductivity sensor [13]. However, the system required the supply of
79 acid and water to sequentially convert the ammonia to ammonium and back to ammonia
80 gas for measurement. In addition, it was only capable of measurement to 1 ppm. Toda *et*
81 *al.* also demonstrated the measurement of ammonia in breath by dissolving it in a droplet
82 of concentrated sulfuric acid on top of a conductivity sensor and demonstrated low ppb
83 level measurement [14]. However, the nature of the device makes it difficult to fabricate
84 and replicate and lacks robustness for everyday diagnostic use. Finally, Gouma *et al.*
85 developed a MoO₃ based nanosensor which was capable of detecting 50 ppbv ammonia in
86 simulated human breath [15]. However, this required operation of the sensor at 500°C,
87 and even then the signal to noise was very poor preventing quantification at these levels.

88 The conducting polymer polyaniline has been identified as an ammonia-sensitive material
89 and this mechanism is reasonably well understood. However, briefly, when doped
90 polyaniline interacts with ammonia, the following reaction occurs:

91



93

94 where PAH^+ and PA are the protonated and deprotonated forms of the polymer,
95 respectively and A^- is the dopant counter anion [16]. This deprotonation of the polymer
96 backbone leads to a decrease in its conductivity which can be measured in a number of
97 ways. Both Kukla *et al.* [16] and Liu *et al.* [17] observed increases in film resistance for
98 polyaniline films exposed to ppm levels of ammonia. Others have used nanocomposites
99 of polyaniline with multi-wall [18] and single-wall [19] carbon nanotubes and titanium
100 dioxide nanoparticles [20] to achieve ammonia measurement down to as low as 25 ppb.
101 However, their application for measurement in breath has not been illustrated. Aguilar *et*
102 *al.* demonstrated the use of polyaniline for the detection of ammonia in breath samples
103 using a nanojunction arrangement with electrodeposited polymer and achieved detection
104 of ammonia to 16 ppb [21]. However, the system also required collection of liquid breath
105 condensate in Tedlar bags and its sequential acidification and neutralisation.

106 Recently, ammonia sensing electrodes using films of inkjet printed polyaniline
107 nanoparticles [22] have been shown to be capable of the measurement of ammonia in air
108 [23] and water [24], with levels of detection down to below 50 ppb using conductance
109 and amperometric techniques. In this work, we demonstrate the application of these

110 polyaniline nanoparticle electrodes to the measurement of ammonia in artificial breath
111 using impedimetric techniques. We demonstrate that impedance could be used to
112 differentiate between changes in temperature, humidity and ammonia and that breath by
113 breath measurement of ammonia was possible across the full diagnostic range using a
114 simple, disposable sensor.

115

116 2. Materials and methods

117 2.1 Materials

118 Polyethylene terephthalate (PET) substrates of 175 μm thickness were supplied by HiFi
119 Industrial Film Ltd., (Dublin, Ireland). Electrodag PF-410 silver ink was supplied by
120 Henkel Ireland Ltd. Dodecylbenzene sulfonic acid (DBSA) was purchased from Tokyo
121 Chemical Industry UK Ltd. Ammonium persulfate (APS), aniline (distilled and stored in
122 nitrogen) and sodium dodecyl sulfate (SDS) were purchased from Sigma-Aldrich Co.
123 (Ireland). Oxygen was provided by Air Products Ireland Ltd (Dublin, Ireland). Nitrogen
124 was produced from in-house generators. Carbon dioxide, ammonia, nitric oxide and
125 hydrogen sulfide gases were supplied by Specialty Gases Ltd (Kent, UK). Deionized
126 water (18 M Ω) was from Veolia Water Solutions and Technologies (Ireland).

127

128 2.2 Instrumentation

129 Screen printing was performed on a DEK-248 screen printer (DEK International, UK).
130 Ink-jet printing was performed using a Dimatix DMP 2831 printer with the Dimatix Drop

131 Manager software (FUJIFILM Dimatix Inc., Santa Clara, CA). Impedance measurements
132 were conducted using a model 660C series electrochemical workstation (CH Instruments
133 Inc., Austin, TX). Simulated breath samples were generated using a combination of
134 respiratory pump and humidifier linked to a microflow controller connected to an
135 ammonia cylinder resulting in a continuous stream of warmed humidified air (62 ± 0.67
136 L/min, $37 \pm 1^\circ\text{C}$, $\geq 90\%$ RH) supplemented with ammonia as appropriate [11]. Ammonia
137 concentrations were calculated from first principles and correlated against photoacoustic
138 laser spectroscopy (Nephrolux, Pranalytica, USA). All gas concentrations were expressed
139 using parts per by volume (ppbv) notation where 1 ppbv ammonia in simulated human
140 breath is equal to approximately $0.67 \mu\text{g}/\text{m}^3$.

141 2.3 Polyaniline nanoparticle synthesis

142 Polyaniline nanoparticles were fabricated according to Ngamna *et al.* [25] In summary,
143 these were synthesized by adding 3.4 g of 0.25 M DBSA to 40 mL of deionized water.
144 This was stirred at 20°C until the DBSA had fully dissolved. To the DBSA solution, 0.36
145 g of APS was added and stirred until fully dissolved. This was followed by 0.6 mL of
146 distilled aniline and was allowed to mix for 2.5 hours. After this time, 20 mL of 0.05 M
147 SDS was added to the DBSA/APS/aniline solution which appeared thick and dark green
148 in colour. The DBSA/APS/aniline/SDS solution was then centrifuged at 5,000 rpm for 30
149 min. The supernatant was transferred to dialysis tubing and dialyzed against 0.05 M SDS
150 for 48 hours. Nanoparticles were characterized by particle sizing and UV-vis
151 spectroscopy. Average particle size was found to be 382 ± 33 nm by dynamic light
152 scattering. Spectroscopy displayed peaks at approximately 350, 430 and 765-790 nm,

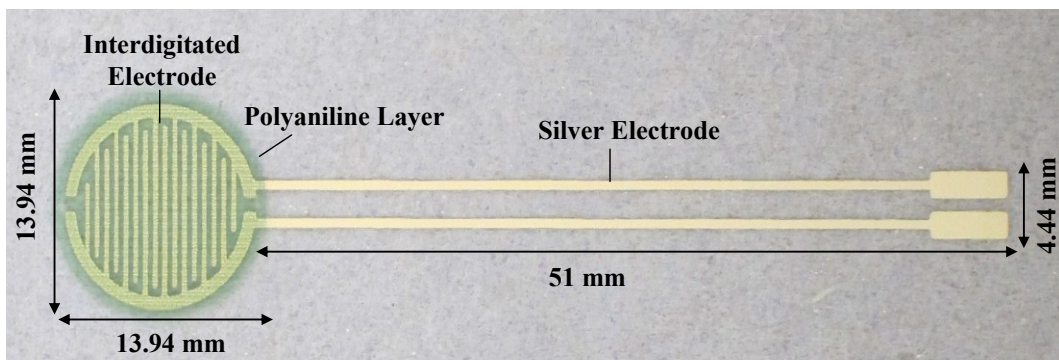
153 indicating π - π^* , π -polaron and localized polaron bands, respectively which was consistent
154 with previous work [25].

155 2.4 Fabrication of sensors

156 Silver interdigitated electrodes were screen printed onto PET using PF-410 cured at
157 120°C for 5 min. A total of ten layers of polyaniline nanoparticle solution were inkjet
158 printed onto the interdigitated electrodes in a circular design of diameter 13.94 mm,
159 covering the entire electrode surface according to Crowley *et al.* [26] The polyaniline
160 nanoparticles were deposited using a 10 pL printer cartridge at 26 V and 5 KHz with a
161 drop spacing of 20 μ m using all 16 nozzles.

162 These were allowed to dry in air and then lightly rinsed with deionized water to remove
163 excess SDS. These were dried at 70°C for 30 minutes (Fig. 1). Polyaniline nanoparticle
164 films were examined by scanning electron microscopy and were found to be comparable
165 to electrodes previously fabricated [22].

166



167

168 Figure 1. Design of the interdigitated polyaniline nanoparticle modified electrode. Screen
169 printed silver interdigitated electrodes were covered with multiple layers of an inkjet
170 printed polyaniline nanoparticle dispersion forming a green film.

171 2.5 Electrode characterization and analysis of ammonia in simulated breath

172 The electrochemical impedance characteristics of the electrodes were investigated in the
173 range of 1 Hz to 100 kHz using a 5 mV rms sinusoidal wave form. Sensors were exposed
174 to streams of air, supplemented with concentrations of ammonia at room temperature and
175 37°C, at ambient and 98% RH or supplemented with other gases. The impedance
176 responses (Z' , Z'' , $|Z|$ and ϕ) of the sensors were analyzed. For final breath analysis,
177 changes in $|Z|$ over time were monitored at 962 Hz and a ratio of the absolute impedance
178 at time t (Z) to the background impedance in air (Z_0) [denoted $(Z/Z_0)-1$] was correlated
179 with ammonia concentration.

180 3. Results and discussion

181 3.1 Electrode Impedance Spectroscopic Characterisation

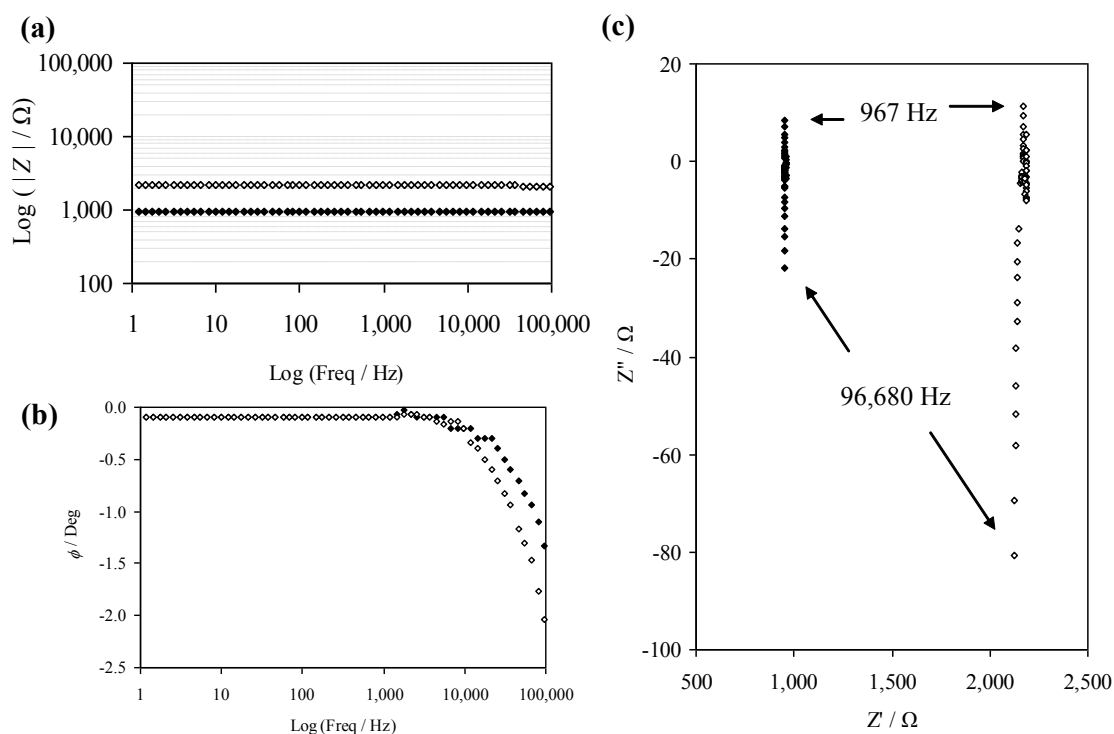
182 As stated, electrodes formed from polyaniline nanoparticles have been investigated for
183 the measurement of ammonia in air and water using conductimetric and amperometric
184 methods [23,24]. However, neither method was ideal as conductivity measurements
185 require perturbation of the system with a bias potential which can lead to modification
186 and degradation of the polymer film, while amperometric methods do not allow
187 continuous monitoring due to the transient nature of the response, while also requiring a
188 three electrode system and not being suitable for gas phase measurement in a two
189 electrode configuration. Impedance techniques have several advantages in that the

190 application of a very small perturbation of the system with a small ac signal ensures that
191 the mean film potential is zero. In combination with interdigitated electrodes, it also
192 becomes very sensitive to changes in both the resistance and capacitance of an
193 immobilised layer. When combined with its spectroscopic capabilities, it can also yield
194 significant electrical and electrochemical information on the nature of the film and its
195 interactions. Thus, the polyaniline nanoparticle-modified electrodes were studied with
196 impedance spectroscopy in the 1 Hz to 100 kHz range to evaluate the impact of exposure
197 of the film to ammonia, changes in temperature, humidity and other potential interfering
198 species. Most impedimetric studies of polyaniline-modified electrodes have employed
199 planar electrodes with electrodeposited polymer in solution [27,28]. Some have also used
200 interdigitated electrodes [29,30], but again, the focus has been on solution-phase
201 experiments in which the solution phase becomes a dominant contribution to the
202 electrical model, as opposed to air, which is an insulating dielectric. This work constitutes
203 the first impedimetric analysis of polyaniline nanoparticle films on interdigitated
204 electrodes measured in air.

205 Bode plot analysis (Fig. 2a) of absolute impedance ($|Z|$) indicated that there was no
206 significant change in the mean $|Z|$ over the range of frequencies in atmospheric air (955
207 $\pm 1.33 \Omega$; $n=3$). However, a noticeable capacitive effect was evident above 962 Hz. This
208 was indicated by a slight decrease in $|Z|$ from 956 to 951 Ω , and a negative change in
209 phase of up to 1.8° at 100 kHz (Fig. 2b). When exposed to ammonia (25 ppmv), the
210 sensors displayed a higher mean $|Z|$ and deviation ($2,166 \pm 17.8 \Omega$; $n=3$). As with the
211 results in air, a capacitive component was also evident above 962 Hz. The impedance

212 decreased from 2,167 to 2,124 Ω , and phase displayed a negative change of up to 2.3° at
213 100 kHz.

214 Nyquist plot analysis (Fig. 2c) also presented a relatively simple impedance profile.
215 Measurement in air showed a series resistance of approximately 1 k Ω and a small
216 capacitance of up to 20 Ω that was apparent at frequencies above 967 Hz. Exposure to
217 ammonia resulted in an increase in the offset series resistance to approximately 2,160 Ω
218 and a slightly elevated change in capacitance of 80 Ω at frequencies above 967 Hz. This
219 data is consistent with a simple equivalent circuit model of a resistor and capacitor in
220 series. This increase in resistance due to the addition of ammonia is consistent with the
221 deprotonation of the film. What may seem more surprising is the low capacitance of the
222 film (20 to 80 nF), given that polyaniline has been investigated extensively as a
223 supercapacitor material [31]. However, this may be due to the nature of the films formed
224 from the deposition of the doped polymer nanoparticles which may result in a low surface
225 concentration of charge sites within the polymer, leading to such low capacitances. Based
226 on these findings, further measurements were performed at 962 Hz at which purely
227 resistive changes due to deprotonation of the film by ammonia would be measured.
228 Analysis of $|Z|$ and ϕ were performed, where appropriate.



229

230 Figure 2. Impedance and phase behavior of polyaniline nanoparticle-modified electrodes
 231 before (filled diamonds) and after (empty diamonds) exposure to 25 ppmv ammonia.
 232 Results over the frequency range of 1 Hz to 100 kHz are indicated by (a) Bode, (b) phase
 233 and (c) Nyquist plots.

234 3.2 Baseline impedance measurement and ratiometric calibration

235 Baseline stability measurements of the electrodes were performed in air for 600 s with a
 236 total of 121 sampling points for each electrode ($n=30$). The time period of 600 s or 10
 237 min. was selected as a suitable time period for the collection of a set of breath
 238 measurements. The mean intra-electrode baseline $|Z|$ ranged from 815 to 2,401 Ω with an
 239 inter-electrode baseline mean and standard deviation of 1,443.7 Ω and 478.2 Ω (rsd =
 240 33%), respectively. Over the 600 s, the intra-electrode drift varied from 1 to 33 Ω (rsd of

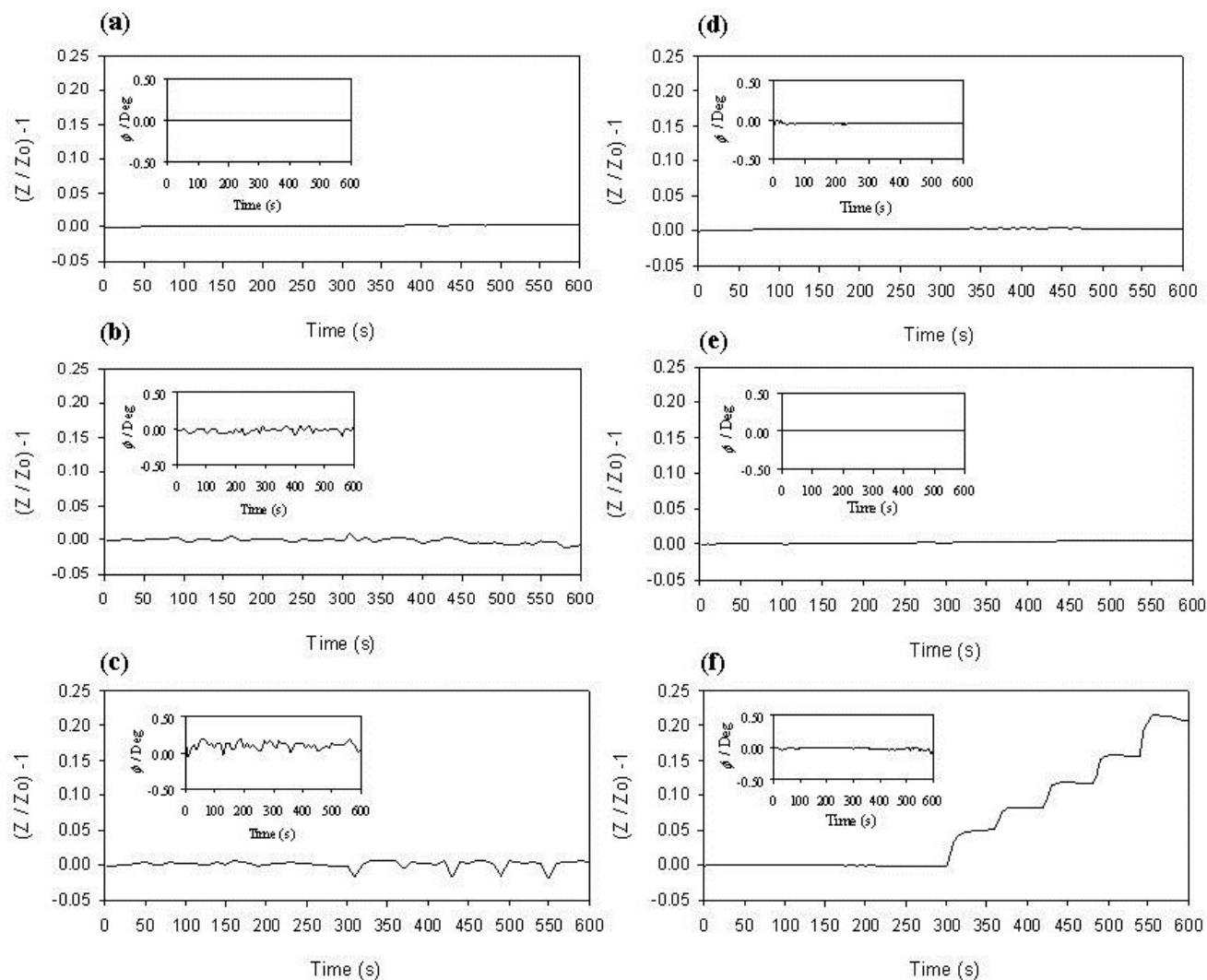
241 0.05 to 1.67%). To compensate for the significant inter-electrode variation in baseline and
242 how this might impact on the reproducibility of ammonia measurement, ten electrodes
243 were analyzed ratiometrically based on their initial baseline impedance in air (Z_0)
244 followed by their measurement upon exposure to simulated breath ammonia (Z). Given
245 that breath samples are pulsatile in nature, an experimental methodology was adopted in
246 which simulated breath samples were pulsed across the electrode, followed by a rest
247 period during which the electrode was only exposed to ambient atmosphere. Following
248 establishment of a baseline $|Z|$ in air for 100 s (Z_0), electrodes were repeatedly exposed to
249 4 s pulses of simulated human breath ($\geq 90\%$ RH, $37 \pm 1^\circ\text{C}$, 62 ± 0.67 L/min) containing
250 ammonia (245 ± 8 ppbv), followed by a gap of 15 s for a period of 500 s. Z/Z_0 was
251 determined to be 2.69 ± 0.12 (rsd=4.46%, n=10). This deviation of less than 5% suggested
252 that the electrodes could be used without the need for extensive individual calibration
253 other than initial ratiometric baseline correction. Further measurements on the electrodes
254 applied this methodology.

255

256 3.3 Evaluation of the Effect of Interferent Gases

257 A major challenge with sensor-based systems and devices is the lack of selectivity of the
258 sensor materials. Polyaniline is no exception and it can be affected in a number of
259 different ways by many species and to varying degrees [32]. Thus, to ensure that it was fit
260 for purpose for breath ammonia measurement it had to be exposed to both ambient
261 atmospheric gases and gases likely to form a part of the exhaled breath sample. The
262 sensor was tested against carbon dioxide (99% (v/v)), nitrogen (99% v/v), oxygen (99%
263 v/v), hydrogen sulfide (25 ppmv) and nitric oxide (25 ppmv). These concentrations were

264 selected as being well beyond levels that would be experienced in air or breath to over-
265 emphasise any potential interfering effects. The gases were used at room temperature and
266 contained no moisture. Figure 3 shows direct exposure of the electrodes to these gases
267 following exposure to atmospheric air for 300 s. Repeated exposure to concentrations of
268 gas at 0.3 L/min flow rates for 4 s intervals were followed by a rest of 60 s. None of these
269 gases showed any significant impedimetric or phase change responses from the
270 electrodes, all at levels that were well above those that would be realistically found in a
271 human breath sample. However, ammonia (25 ppmv) exhibited an increase in Z/Z_0 with
272 no significant change in phase. This change was consistent with earlier impedimetric
273 analysis and previous literature [33-35]. Analysis of carbon dioxide, nitric oxide and
274 hydrogen sulfide in warmed humidified air showed similar response patterns to those
275 shown, demonstrating no additional contribution from humidity or temperature to the
276 interfering effect of these gases (data not shown).



277

278 Figure 3. Ratiometric impedance $[(Z/Z_0)-1]$ and phase (ϕ) (inset) responses of the
 279 polyaniline nanoparticle-modified electrodes to potential interferent gases in human
 280 breath: (a) 99% (v/v) carbon dioxide, (b) 99% (v/v) nitrogen, (c) 99% (v/v) oxygen, (d)
 281 25 ppmv hydrogen sulfide, (e) 25 ppmv nitric oxide, (f) 25 ppmv ammonia (n=3).

282

283 Polyaniline has been shown to be responsive to CO_2 [36]. However, this has been while
 284 in its de-doped, base form whereupon, the carbonate ion acts as a dopant and causes the

285 film to re-protonate. Emeraldine salt forms of the polymer are thus unresponsive to CO₂
286 as observed here as they are already significantly doped, in this case with DBSA. The
287 application of polyaniline base for CO₂ sensing has also been disputed [29].

288

289 A great deal of work has looked at the interaction of oxygen and polyaniline, principally
290 with polyaniline acting as a cathode in the reduction of oxygen. Typically, the onset of
291 oxygen reduction at polyaniline-modified electrodes is -0.4 V [37], and so should not
292 contribute significantly to impedance measurements performed at 0 V, as is the case here.
293 The inert nature of nitrogen also makes it unlikely that it would interact significantly with
294 polyaniline, other than displace other species such as water that may show some effect.
295 However, this was not the case.

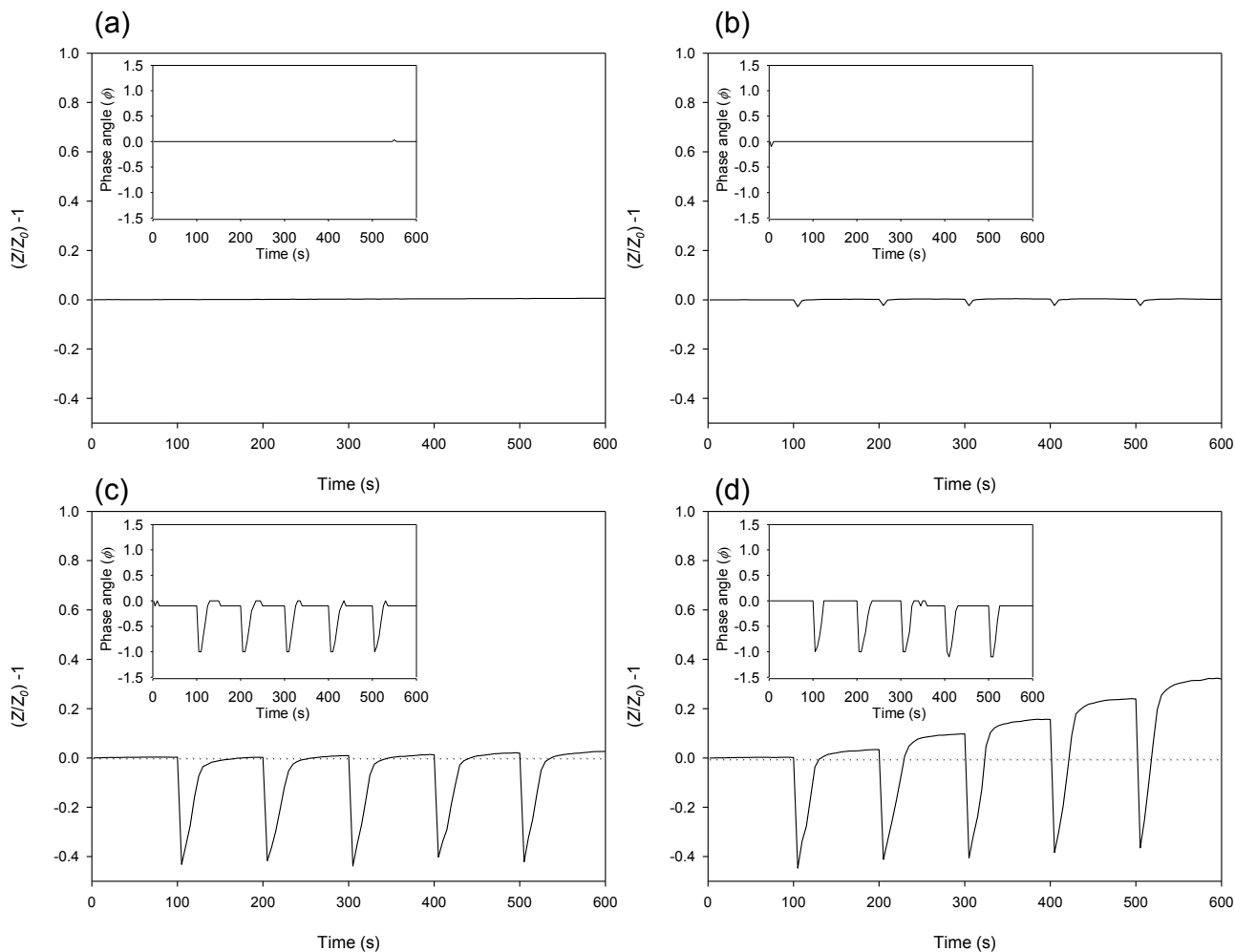
296 Work with hydrogen sulfide has shown both significant increases and decreases in
297 conductivity depending on the composition of the polyaniline [26]. The emeraldine salt
298 form of polyaniline has shown weak responses to hydrogen sulfide. However, it was
299 noted that both base-treated polyaniline and copper chloride composite polyaniline
300 displayed significant increases in conductivity. This behavior was similar to the
301 previously discussed base-treated polyaniline and indicated that the polyaniline had been
302 protonated to the salt form. Again, the doped emeraldine form used here also showed no
303 response to hydrogen sulfide, which was consistent with these findings.

304 From this, it was deduced that ammonia was the only major gas in breath that would have
305 a significant effect on the polyaniline nanoparticle-modified electrodes. However, given

306 that real breath contains many more trace volatiles, further studies would be required to
307 show if other gases at diagnostically relevant concentrations might result in interference.

308 3.4 Evaluation of the Effects of Temperature and Humidity

309 Tests were performed to evaluate the effect of atmospheric air at room temperature (21
310 $\pm 1^\circ\text{C}$), atmospheric air at human breath temperature ($37 \pm 1^\circ\text{C}$), humidified air at human
311 breath temperature ($37 \pm 1^\circ\text{C}$, $\geq 90\%$ RH), and humidified air at human breath temperature
312 containing ammonia ($37 \pm 1^\circ\text{C}$, $\geq 90\%$ RH, 245 ± 8 ppbv) on the ratiometric impedimetric
313 response of the polyaniline nanoparticle-modified electrodes (Fig. 4). Over a time span of
314 600 s, the first 100 s were again used as the baseline in atmospheric air. Subsequently, the
315 electrodes were exposed to a simulated breath sample for repeated periods of 4 s every
316 100 s.



317

318 Figure 4. Polyaniline nanoparticle-modified electrode ratiometric impedance responses
 319 $[(Z/Z_0)-1]$, and phase angle (ϕ) (inset) to (a) room temperature atmospheric air, $21 \pm 1^\circ\text{C}$,
 320 (b) warmed atmospheric air ($37 \pm 1^\circ\text{C}$), (c) warmed humidified atmospheric air ($37 \pm 1^\circ\text{C}$,
 321 $\geq 90\%$ RH) and (d) warmed humidified air with ammonia ($37 \pm 1^\circ\text{C}$, $\geq 90\%$ RH, 245 ± 8
 322 ppbv).

323

324 As might be expected due to the fact that they had already been equilibrated in
 325 atmospheric air, the electrodes exposed to a flow of atmospheric air showed no

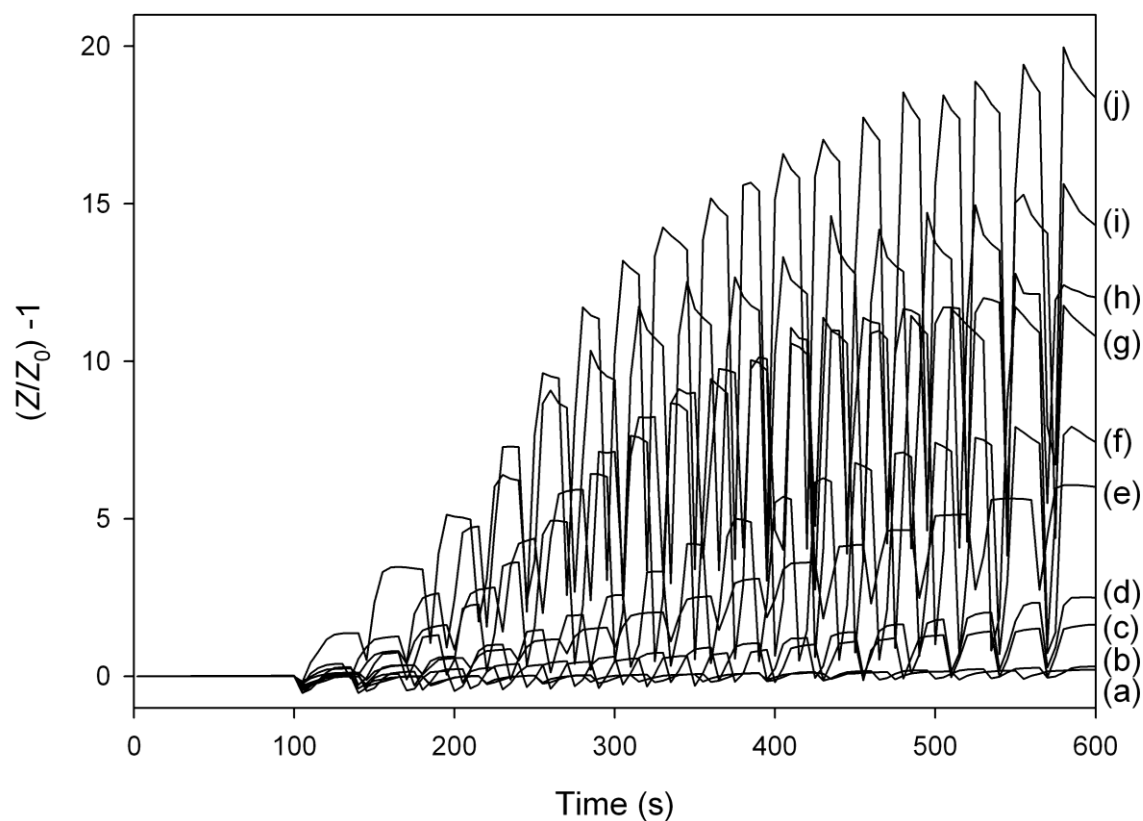
326 significant change in ratio-metric impedance, $[(Z/Z_0-1)]$, or φ (Fig. 4a). Atmospheric air
327 warmed to a temperature comparable to that of human breath (Fig. 4b) was detected by
328 the sensor with a very negligible and transient decrease in Z/Z_0 , with no observable
329 change in φ . These findings were similar to those seen elsewhere reporting slight changes
330 in conductivity of polyaniline in the range from room temperature to approximately 60°C
331 [23]. When application of the simulated breath sample was removed, the original baseline
332 was rapidly restored as the electrode temperature returned to its original level. However,
333 heated humidified air (Fig. 4c) resulted in a significant transient decrease in Z/Z_0 .
334 Furthermore, there was also a noticeable change in phase angle indicating both a change
335 in film resistance and capacitance due to exposure to water vapour. Again, following
336 removal of application of the sample and as the water vapour evaporated from the
337 electrode, $|Z|$ and the φ both returned to their original baselines in a characteristic, time-
338 dependent manner. The effect of temperature and humidity changes on the resistance of
339 polyaniline nanomaterials has been observed elsewhere [38]. In humidified air at human
340 breath temperature containing ammonia (Fig. 4d), the interaction of humidity with the
341 electrodes again caused a negative phase shift and an initial decrease in Z/Z_0 , similar to
342 Fig. 4c. However, upon recovery of the electrode from the temperature and humidity
343 effects, an increase in the Z/Z_0 level could be observed, whereas no permanent change in
344 the phase angle was apparent. This suggested that, at this frequency, the ammonia brought
345 about a change in the resistance of the electrodes, whereas water vapour contributed both
346 transient resistive and capacitive effects. This indicated that the impedimetric response
347 signature of ammonia on the electrodes could be differentiated from temperature and
348 humidity components by time-dependent control of the sampling methodology, or

349 through differential analysis of the changes in impedance and phase. For the present
350 work, a time-controlled breath sampling method was employed.

351

352 3.5 Quantification of Ammonia in Simulated Human Breath

353 The polyaniline nanoparticle-modified electrodes were exposed to 16 sequential
354 simulated breath samples ($\geq 90\%$ RH, $37 \pm 1^\circ\text{C}$, 62 ± 0.67 L/min) containing ammonia at
355 concentrations from 40 ± 2 ppbv to $2,175 \pm 26$ ppbv. Electrodes were repeatedly exposed
356 to 4 s intervals of sample breath gas, followed by a 26 s delay over a 600 s period (Fig. 5).



357

358 Figure 5. Ratiometric impedance response $[(Z/Z_0)-1]$ profile of simulated breath samples
359 of 4 s duration on polyaniline nanoparticle-modified electrodes measured at 962 Hz. The
360 ammonia concentrations were: (a) 40 ± 2 ; (b) 121 ± 15 ; (c) 245 ± 8 ; (d) 392 ± 6 ; (e) 755 ± 7 ;
361 (f) 984 ± 21 ; (g) $1,368 \pm 11$; (h) $1,576 \pm 7$; (i) $1,919 \pm 20$; and (j) $2,175 \pm 26$ ppbv.

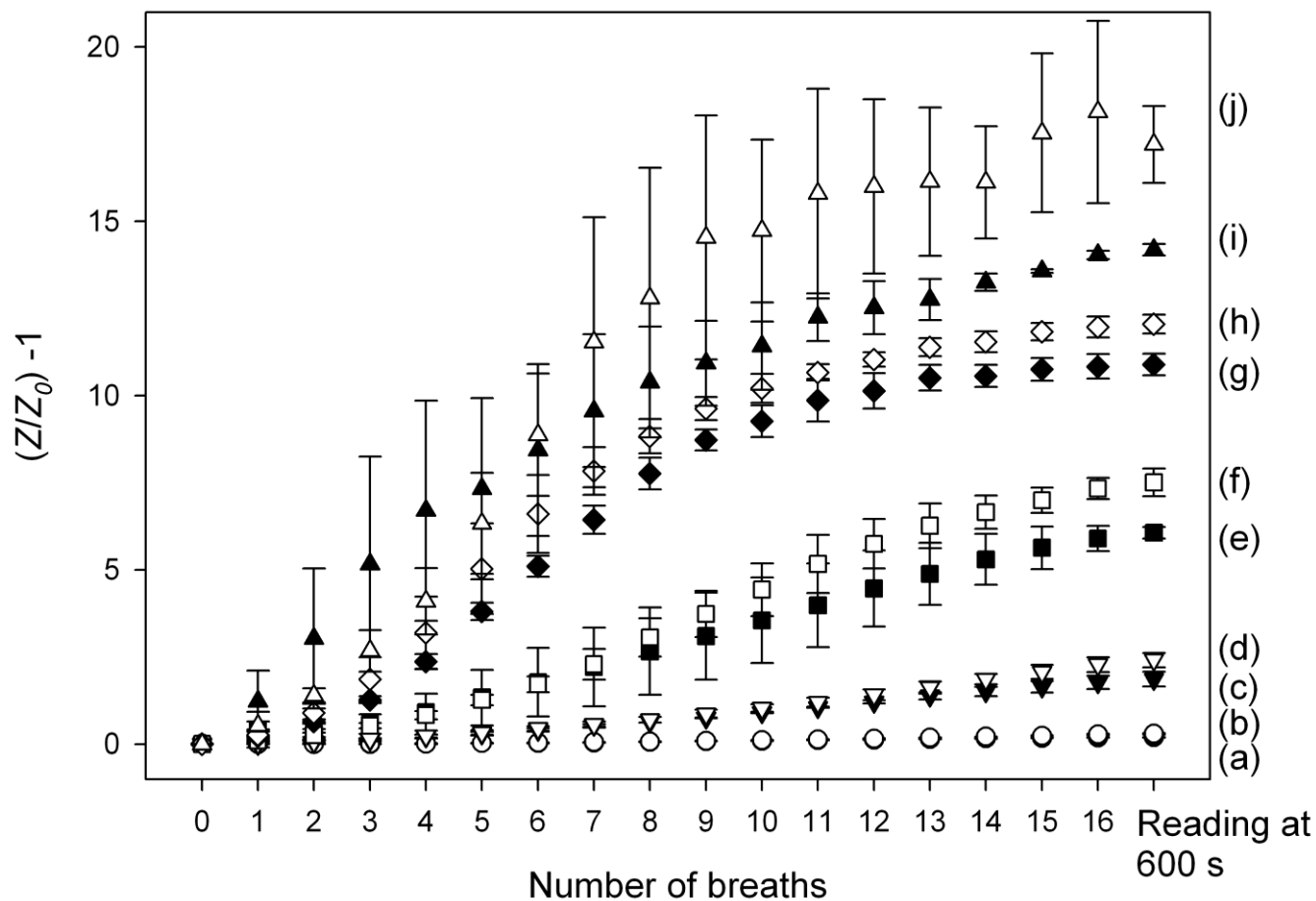
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363 The characteristic transient decrease in $(Z/Z_0)-1$ which was shown to be due to
364 temperature and humidity could be observed while the simulated breath sample was being
365 passed over the sensor. In a similar manner to that shown in Fig. 4d, cumulative increases
366 in $(Z/Z_0)-1$ could be observed for all concentrations of ammonia. It could also be observed
367 that the dissociation of ammonia from the film, as evidenced by the subsequent decrease
368 in $(Z/Z_0)-1$ becomes more apparent as the concentration increases. Thus, after a specified
369 number of breaths at controlled flow rate (and sample volume), with defined sampling
370 gaps, the change in $(Z/Z_0)-1$ was proportional to the ammonia concentration.

371

372 Peak responses following each simulated breath were averaged ($n=3$) and plotted to
373 determine the effect of sampling time and the number of cumulative breaths on assay
374 range and linearity (Fig. 6). The changes in Z/Z_0 were observed for each ammonia
375 concentration at every 30 s interval. This showed that the relationship between response
376 and breath number was largely linear for all concentrations until approximately 8 breaths.
377 At higher ammonia concentrations, there was a significant deviation from linearity which
378 is likely to be due to saturation of the polymer with ammonia which may indicate a

379 progression from surface saturation to bulk saturation. Higher ammonia concentrations
 380 also exhibited a greater inter-electrode variability.



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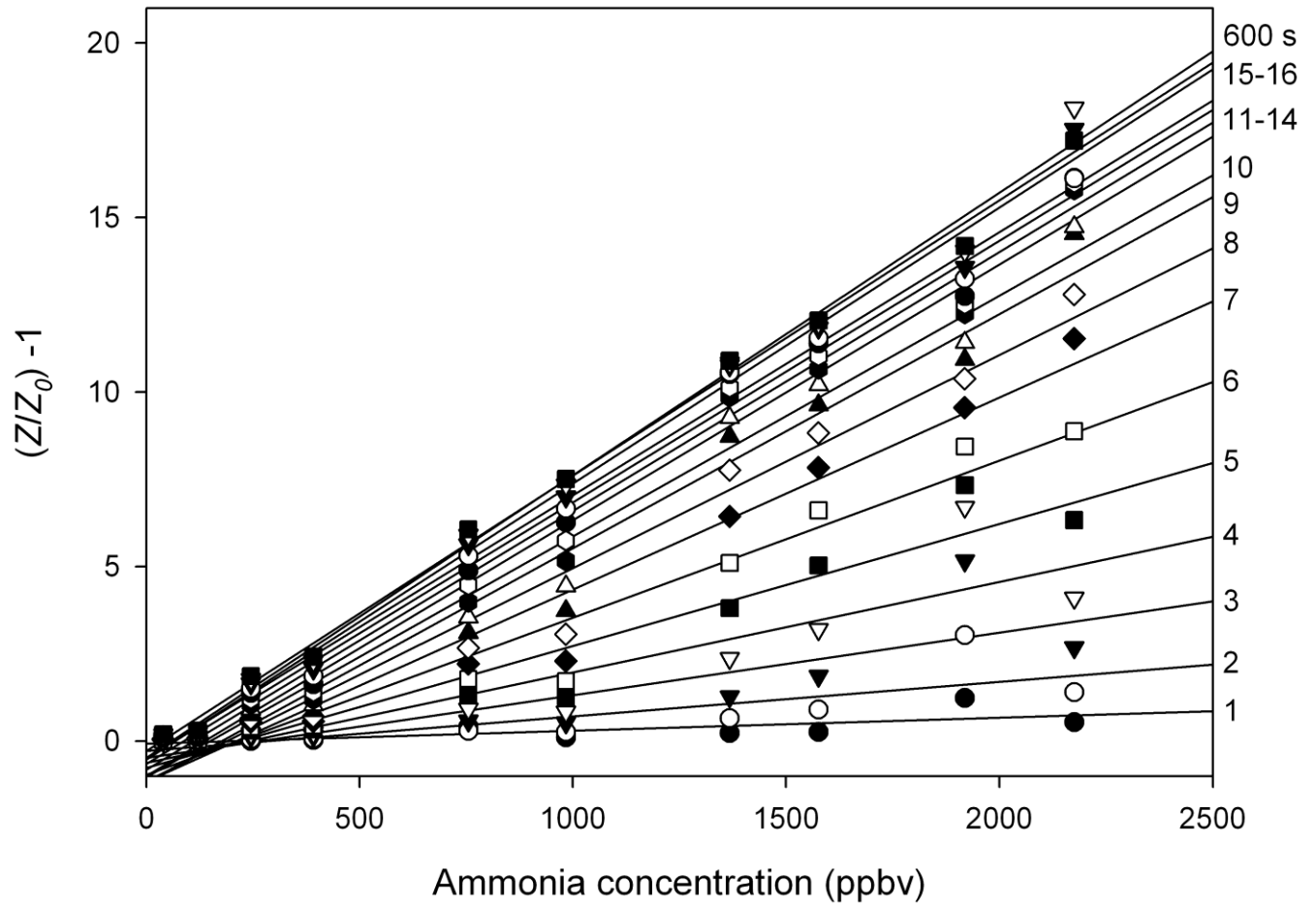
382 Figure 6. Relationship between ratiometric impedance response and number of
 383 cumulative simulated breaths of 4 s duration. Ammonia concentrations were: (a) 40 ± 2 ;
 384 (b) 121 ± 15 ; (c) 245 ± 8 ; (d) 392 ± 6 ; (e) 755 ± 7 ; (f) 984 ± 21 ; (g) $1,368 \pm 11$; (h) $1,576 \pm 7$;
 385 (i) $1,919 \pm 20$ and; (j) $2,175 \pm 26$ ppbv.

386

387 Calibration curves of ammonia concentration vs. impedance response for each number of
388 breaths are shown in Figure 7. The response was found to be linear across the full assay
389 range tested from 40 to 2,175 ppbv ammonia. However, the sensitivity of the response
390 was extremely poor after a single breath measurement. This improved significantly up to
391 approximately 8 breaths at which the polymer film was not yet nearing saturation from
392 ammonia at the higher concentrations. Above this number of breaths, there were no
393 further significant increases in slope. However, the linear regression coefficients between
394 ammonia concentration and Z/Z_0 improved with respect to increased breath number
395 (Table 1). The correlation coefficient was found to be only 0.5584 after a single breath.
396 However, after 16 breaths and measurement at 600 s, this had increased to 0.9963. This
397 increase may be due to the cumulative nature of the sampling methodology as a larger
398 number of samples would average out any sample-to-sample variations, while also
399 benefitting from improved response sensitivity and inherently better signal-to-background
400 ratios.

401

402 A final measurement at 600 s gave a slope and intercept of 0.0079 ppbv^{-1} and -0.3 ,
403 respectively, and the rsd of the replicates varied between 1.17 and 11.22% ($n=3$) (Fig. 8).
404 Based on this data in combination with the intra-electrode baseline drift variability
405 determined earlier, a theoretical limit of detection of approximately 6.2 ppbv could be
406 determined ($S/N=3$) with linearity to 2,175 ppbv ammonia and beyond. This is
407 appropriate for the measurement range required in diagnostic breath measurements of
408 both normal populations and patients with elevated ammonia levels [10].



409

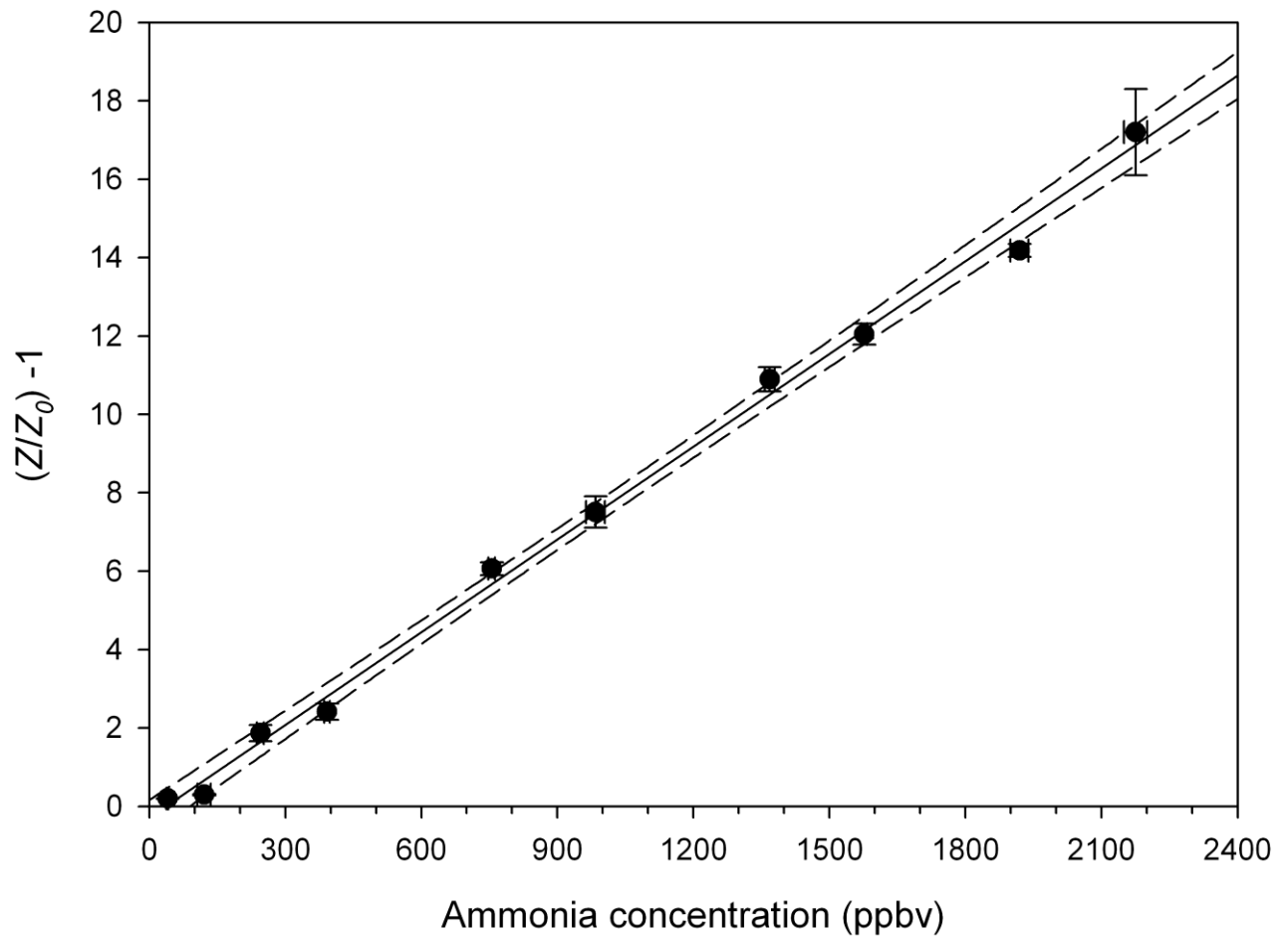
410 Figure 7. Relationship between ratiometric impedance response and ammonia
 411 concentration with respect to the number of cumulative breaths (1-16) sampled. The value
 412 of 600 s indicates a final measurement at this time.

413

414 Table 1. Linear least squares regression coefficients between ratiometric impedance
 415 response and simulated breath ammonia concentration with respect to the number of
 416 breaths sampled.

Breath Number	Correlation (R^2)	Breath Number	Correlation (R^2)
1	0.5584	9	0.9698
2	0.6475	10	0.9788
3	0.7102	11	0.9837
4	0.8083	12	0.9882
5	0.9257	13	0.9901
6	0.9529	14	0.9942
7	0.9604	15	0.9920
8	0.9694	16	0.9923
		600 s	0.9963

417



418

419 Figure 8. Relationship between ammonia concentration and ratiometric impedance
 420 response after 16 simulated breath samples measured at 600 s ($R^2 = 0.9963$). A slope and
 421 intercept of 0.0079 ppbv^{-1} and -0.2852 were determined. 95% confidence interval (dashed
 422 line).

423

424 4. Conclusions

425 An electrode based on an inkjet-printed polyaniline nanoparticle film could be used for
 426 the measurement of ammonia in simulated breath. Impedance analysis established a

427 calibration-free measurement methodology based on ratio-metric measurement of
428 absolute impedance at 962 Hz, 5 mV rms. The sensor was shown to be free of
429 interference from the major gaseous constituents of breath. Effects of temperature and
430 water vapour could also be differentiated from the measurement of ammonia. This
431 allowed the quantitative measurement of ammonia in simulated breath samples across the
432 diagnostically relevant range and demonstrates that these sensors may have potential for
433 measurement of ammonia in human breath for diagnostic applications.

434

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